

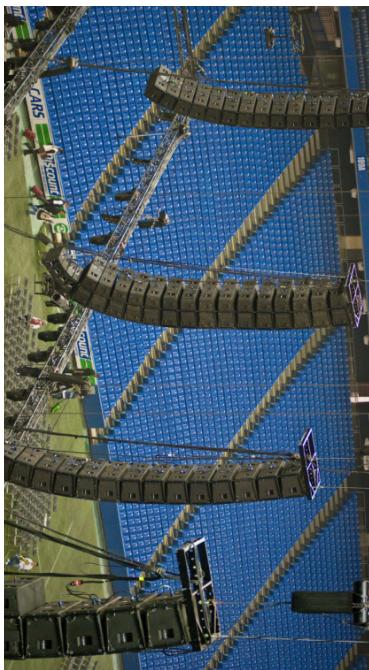


On Spatial-Aliasing-Free Sound Field Reproduction using Infinite Line Source Arrays

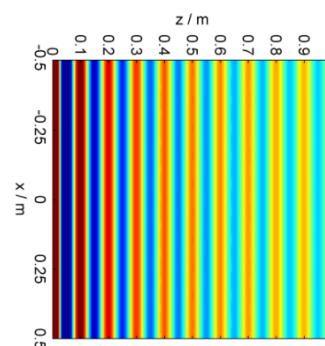
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Institute of Communications Engineering

136th AES Convention, Berlin
2014-04-29 10:00, paper session P11 "Spatial Audio", #9078

Introduction Line Source Array Application



No spatial aliasing



Line Source Array Element



Spatial aliasing

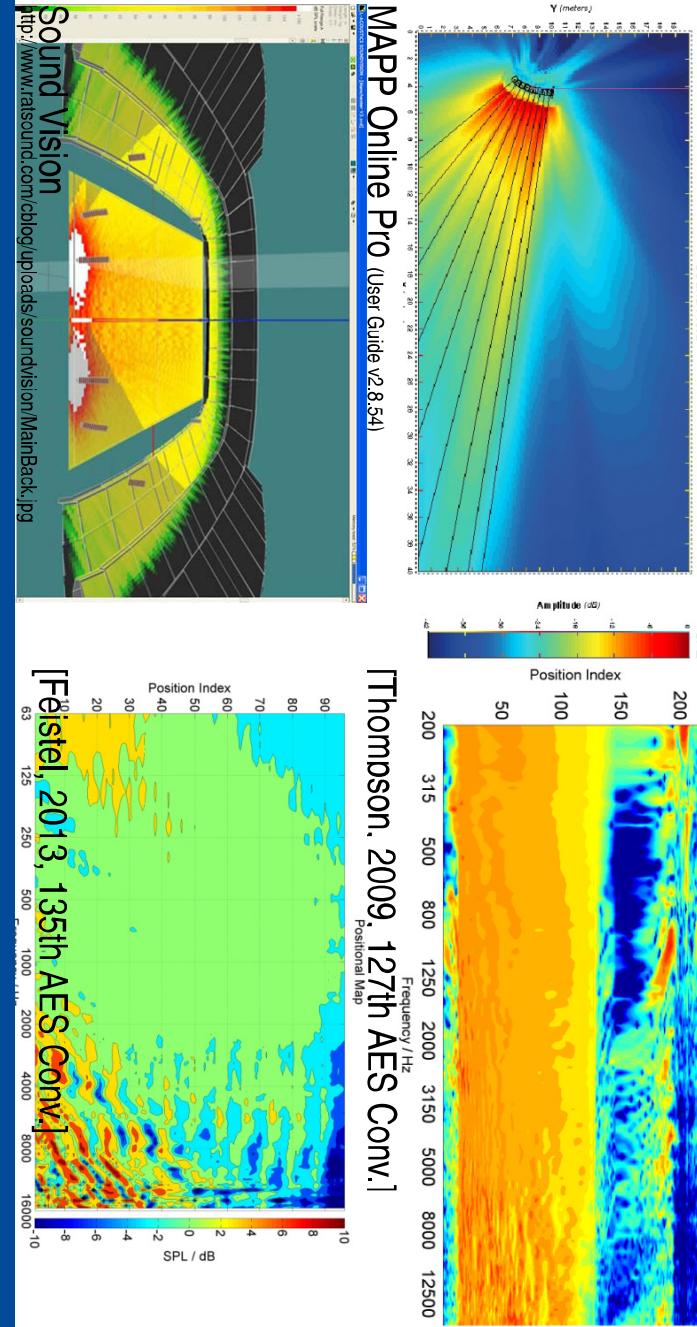


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Line Source Array Prediction

[Feistel, 2009, JAES 57(6)]

$$\underbrace{P(\mathbf{x}, \omega)}_{\text{sound pressure}} = \sum_{n=1}^N \underbrace{D(\mathbf{x}_0, n, \omega)}_{\text{filter}} \underbrace{A_n(\mathbf{x}, \mathbf{x}_0, n, \omega)}_{\text{directivity}} \underbrace{\frac{e^{-j \frac{\omega}{c} |\mathbf{x} - \mathbf{x}_0, n|}}{4 \pi |\mathbf{x} - \mathbf{x}_0, n|}}_{\text{monopole}}$$



Wavefront Sculpture Technology® (WST)

[Heil, 1992, 92nd AES Conv.]

[Urban, 2001/2003, 111th AES Conv./JAES 51(10)]

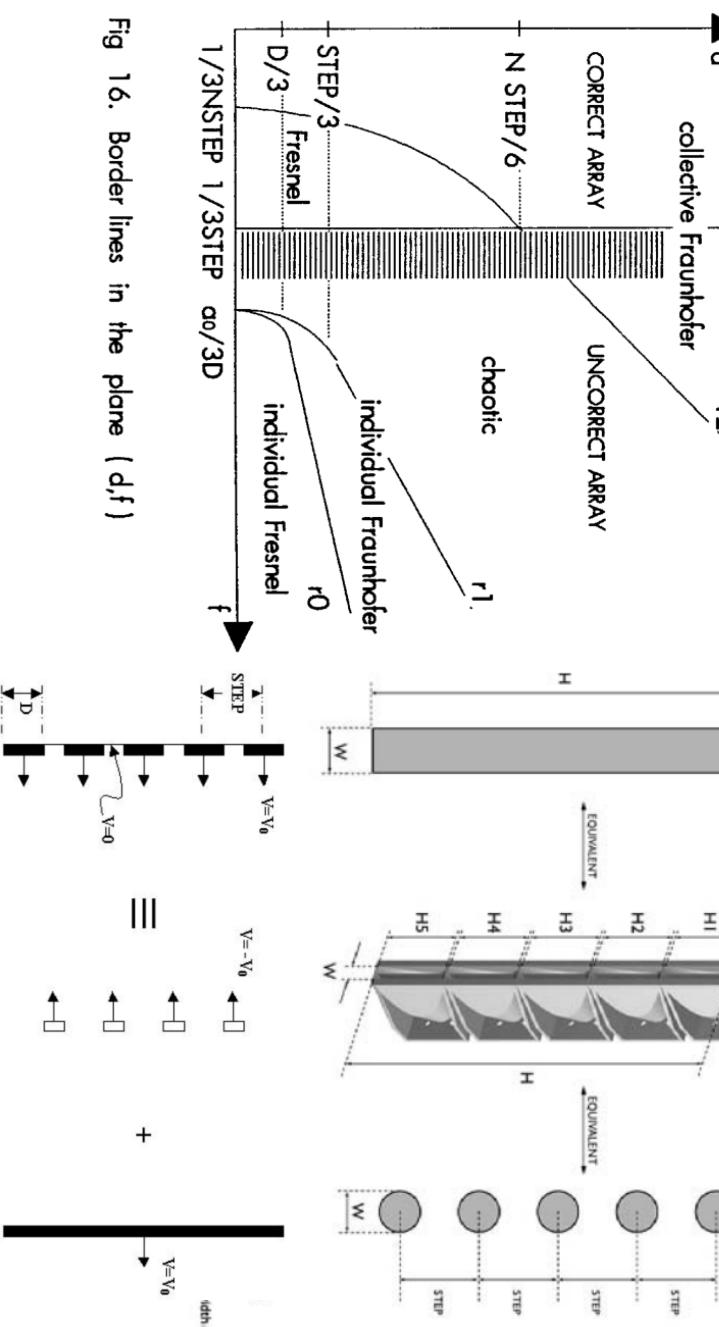


Fig 16. Border lines in the plane (d,f)

[Ureda, 2004, JAES 52(5)]

Schultz, Rettberg, Spors | Spatial-Aliasing-Free Line Source Arrays

Motivation

Real array
≡ Disruption grid
+ In phase opposition
= Continuous line source
+- Line source

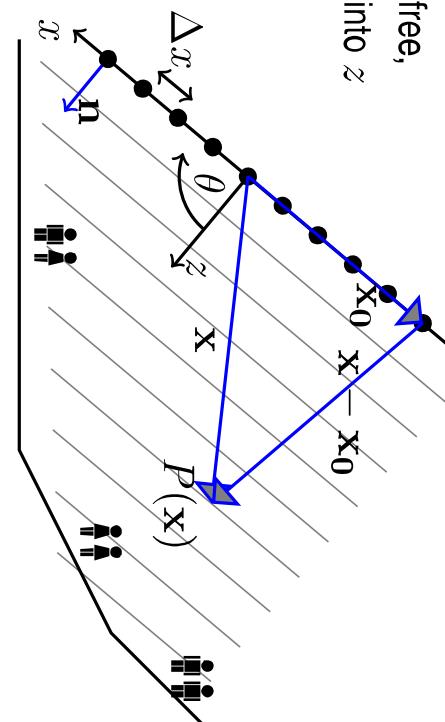
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Problem Formulation

$$\underbrace{P(\mathbf{x}, \omega)}_{\text{sound pressure}} = \sum_{n=1}^N \underbrace{D(\mathbf{x}_0, \mathbf{n}, \omega)}_{\text{filter}} A_n(\mathbf{x}, \mathbf{x}_0, \mathbf{n}, \omega) \underbrace{\frac{e^{-j \frac{\omega}{c} |\mathbf{x} - \mathbf{x}_0, \mathbf{n}|}}{4 \pi |\mathbf{x} - \mathbf{x}_0, \mathbf{n}|}}_{\text{loudspeaker}}$$

$$\underbrace{P(\mathbf{x}, \omega)}_{\text{sound pressure}} = \int_{-\infty}^{+\infty} \underbrace{D_{\text{sampled}}(\mathbf{x}_0, \omega)}_{\text{driving function}} \cdot \underbrace{G(|\mathbf{x} - \mathbf{x}_0|, \omega)}_{\text{loudspeaker}} d\mathbf{x}_0$$

Aim: spatial-aliasing free,
cylindrical wavefront into z



Signal Processing Model for Sound Field Synthesis

- Continuous problem formulation with monopoles

$$\underbrace{P(\mathbf{x}, \omega)}_{\text{sound pressure}} = \int_{-\infty}^{+\infty} \underbrace{D(\mathbf{x}_0, \omega)}_{\text{driving function}} \cdot \underbrace{G(|\mathbf{x} - \mathbf{x}_0|, \omega)}_{\text{monopole}} d\mathbf{x}_0$$

- Interpretation as a spatial convolution along x_0

$$P(\mathbf{x}, \omega) = D(\mathbf{x}, \omega) *_{x_0} G(|\mathbf{x} - \mathbf{0}|, \omega)$$

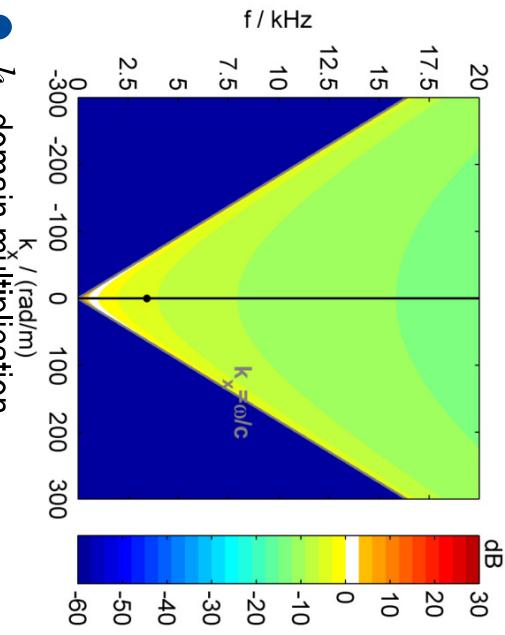
- This corresponds to a multiplication in the k_x -domain

$$P(k_x, 0, z, \omega) = D(k_x, 0, z, \omega) \cdot G(k_x, 0, z, \omega)$$

using the one-dimensional spatial Fourier transform along x_0

$$P(k_x, 0, z, \omega) = \int_{-\infty}^{+\infty} P(x, 0, z, \omega) e^{+j k_x x} dx$$

Signal Processing Model for Sound Field Synthesis



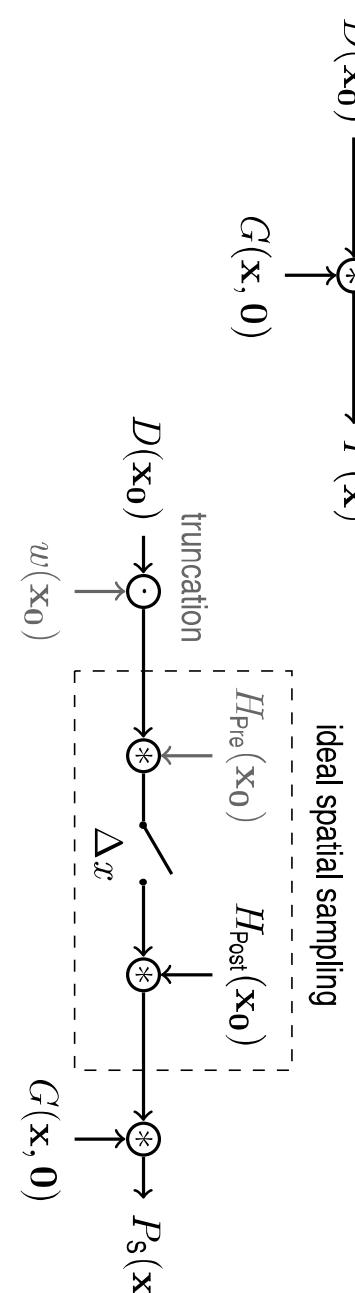
- k_x -domain multiplication

$$P(k_x, 0, z_{\text{ref}}, \omega) = D(k_x, 0, z_{\text{ref}}, \omega) \cdot G(k_x, 0, z_{\text{ref}}, \omega)$$

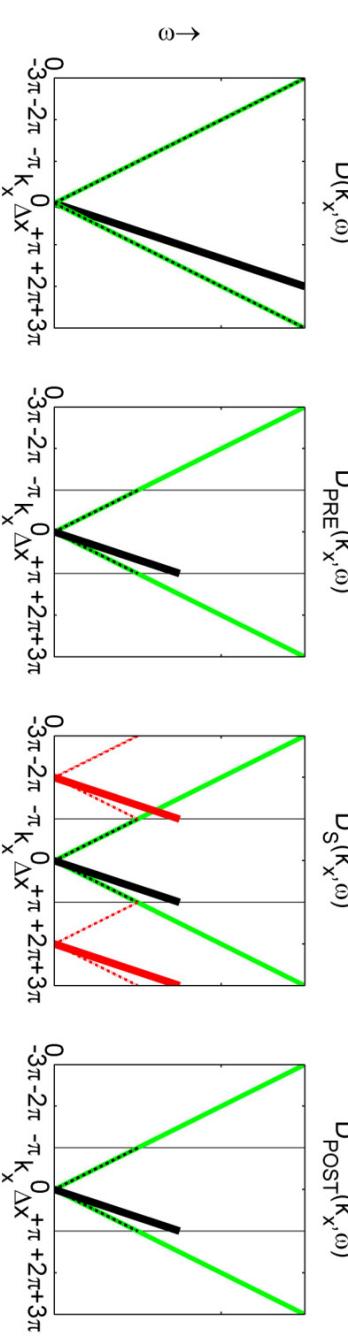
- Dispersion relation for a 2.5D wave propagation problem, $k_x = \frac{\omega}{c} \sin \theta$

$$\left(\frac{\omega}{c}\right)^2 = k_x^2 + k_z^2 \quad \text{we want: } k_x = 0$$

Baseband Sampling for Spatial Signals



$$\Delta x \circ \bullet \Delta k_x = \frac{2\pi}{\Delta x}$$

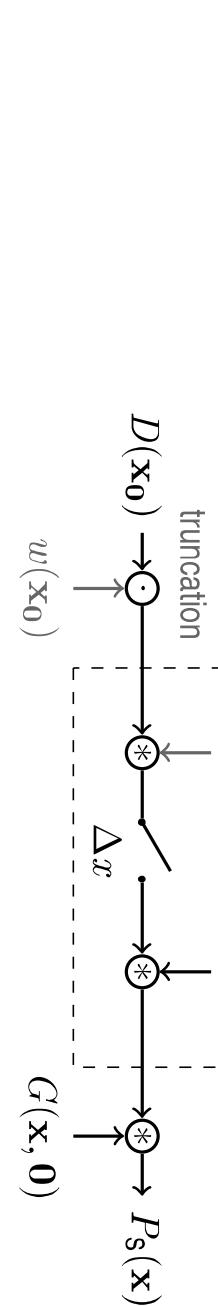


Baseband Sampling for Spatial Signals

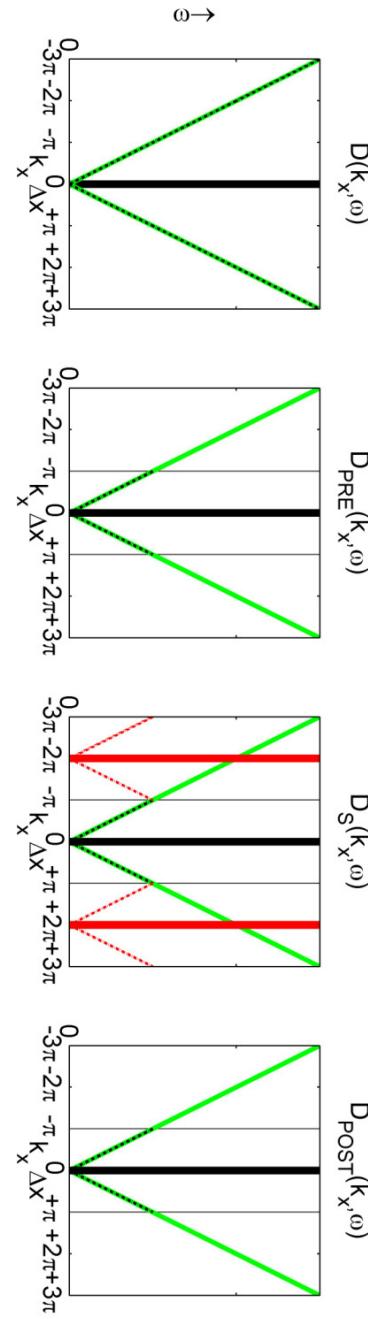
$$D(\mathbf{x}_0) \xrightarrow{*} P(\mathbf{x})$$

$$G(\mathbf{x}, 0)$$

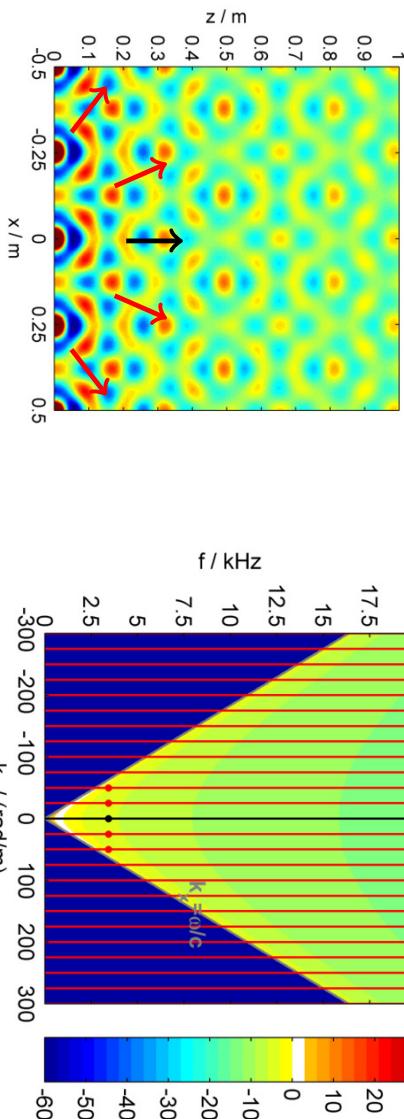
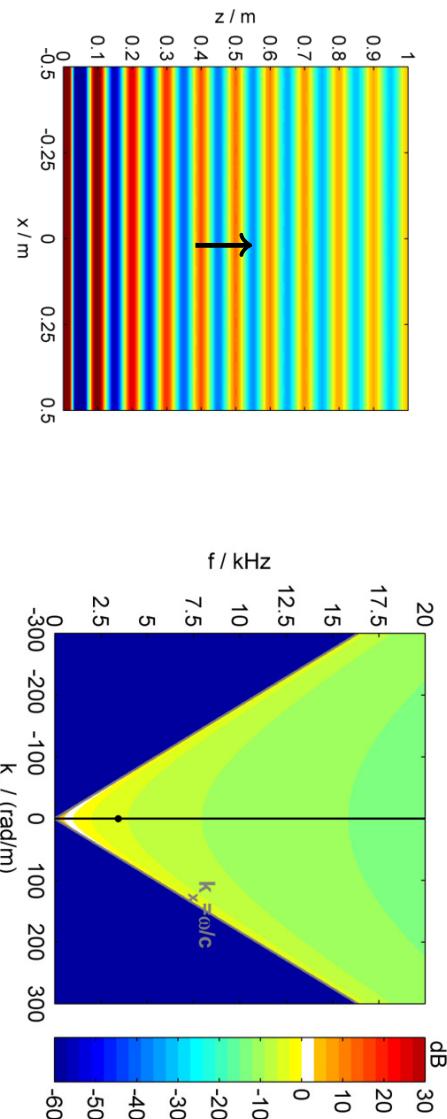
ideal spatial sampling



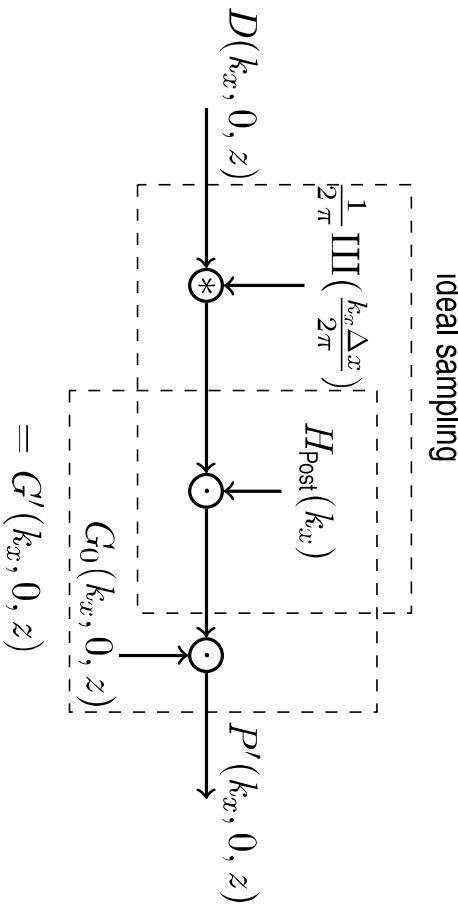
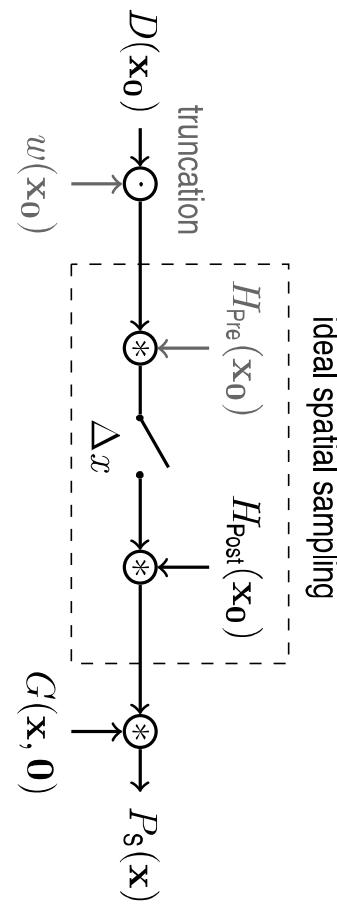
$$\Delta x \circ \bullet \quad \Delta k_x = \frac{2\pi}{\Delta x}$$



Spatial Aliasing due to missing Spatial Postfilter



Baseband Sampling for Spatial Signals



Use the Loudspeaker as the Spatial Postfilter

model $H_{\text{Post}}(k_x)$ with the farfield directivities of a loudspeaker
farfield directivities have spatial lowpass characteristics

circular piston with radius r_0

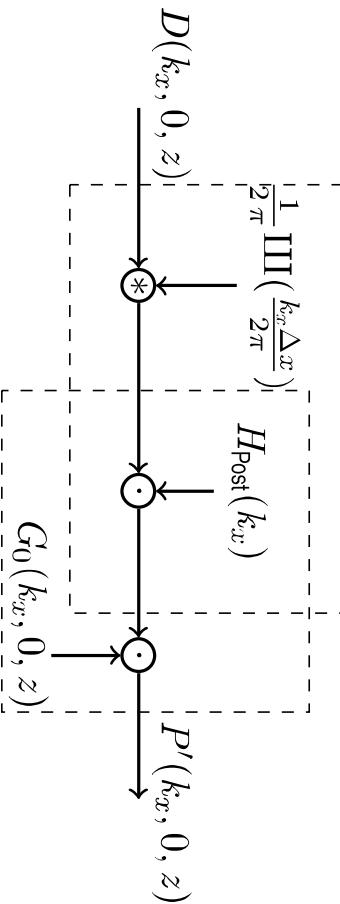
line piston with length L

$$H_{\text{Circ}}(k_x) = \frac{2 J_1(\frac{\omega}{c} \sin \theta r_0)}{\frac{\omega}{c} \sin \theta r_0}$$

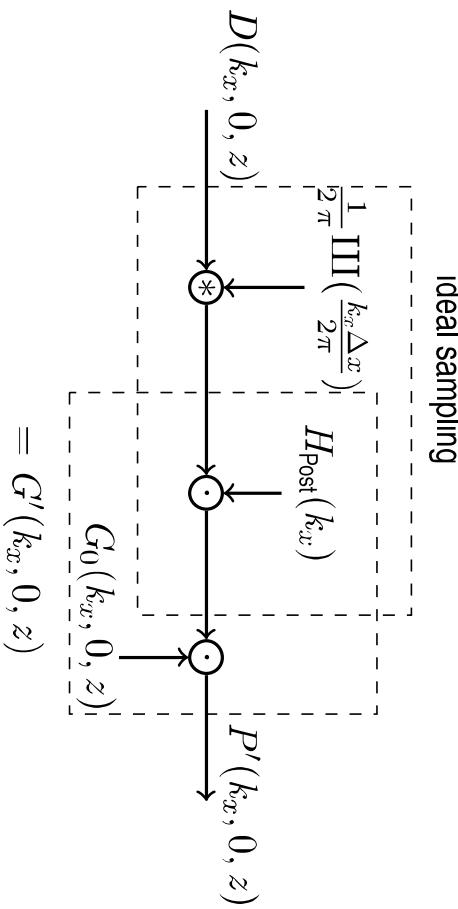
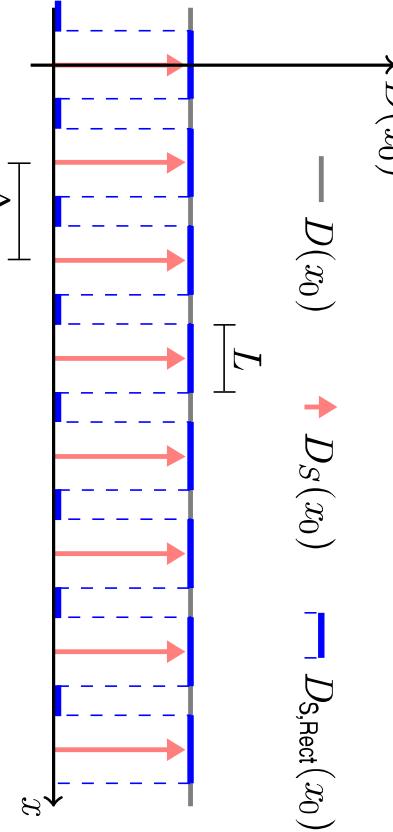
$$H_{\text{Rect}}(k_x) = \frac{\sin \left(\frac{\omega}{c} \sin \theta \frac{L}{2} \right)}{\frac{\omega}{c} \sin \theta \frac{L}{2}}$$

$$k_x = \frac{\omega}{c} \sin \theta$$

ideal sampling



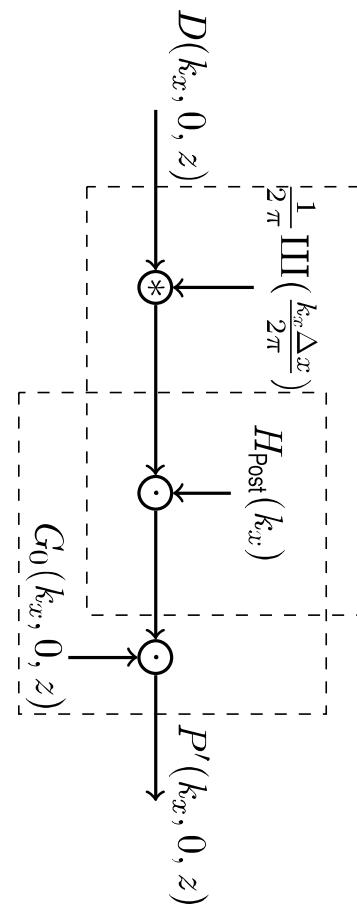
Waveguide as a Spatial Lowpass Filter



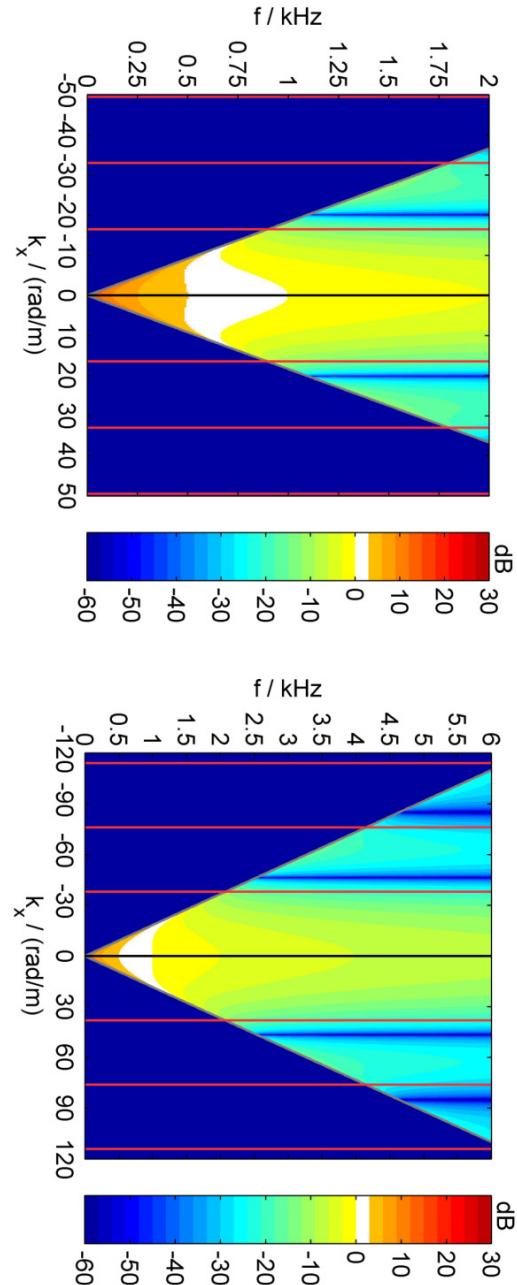
Line Array Prediction vs. Signal Model

$$\underbrace{P(\mathbf{x}, \omega)}_{\text{sound pressure}} = \sum_{n=1}^N \underbrace{D(\mathbf{x}_0, \mathbf{n}, \omega)}_{\text{filter}} \underbrace{A_n(\mathbf{x}, \mathbf{x}_0, \mathbf{n}, \omega)}_{\text{directivity}} \underbrace{\frac{e^{-j \frac{\omega}{c} |\mathbf{x} - \mathbf{x}_0, \mathbf{n}|}}{4\pi |\mathbf{x} - \mathbf{x}_0, \mathbf{n}|}}_{\text{monopole}}$$

ideal sampling



Circular Piston Model



$$d = \Delta x = 15"$$

suitable for lowest frequencies < 500Hz

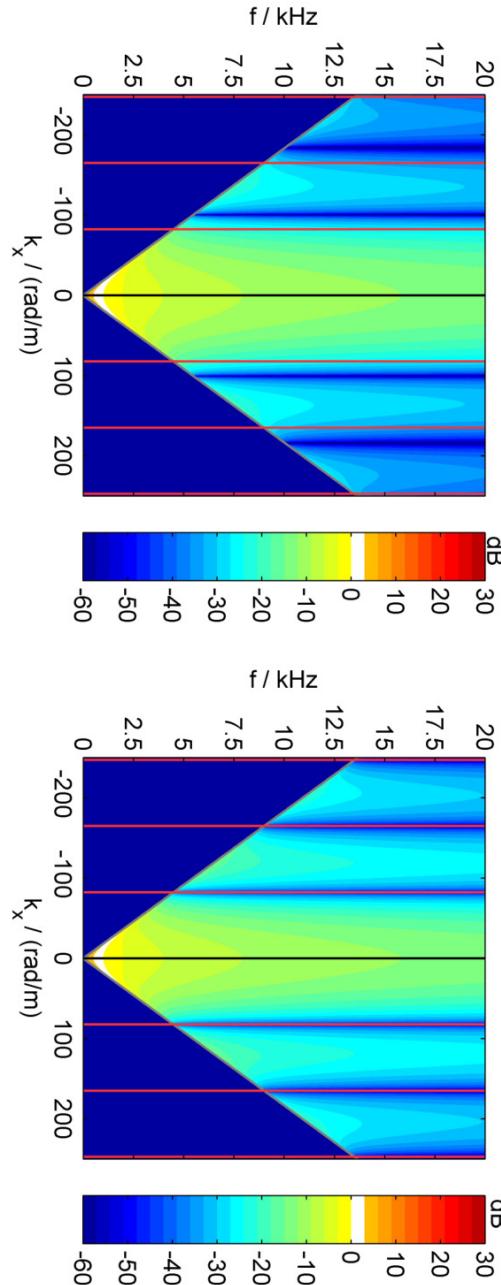
speaker's diameter d



[http://www.electrovoice.com/
downloadfile.php?f=XLC.Brochure_](http://www.electrovoice.com/downloadfile.php?f=XLC.Brochure_FI.pdf)
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Circular vs. Line Piston Model



circular piston

$$d = \Delta x = 3"$$

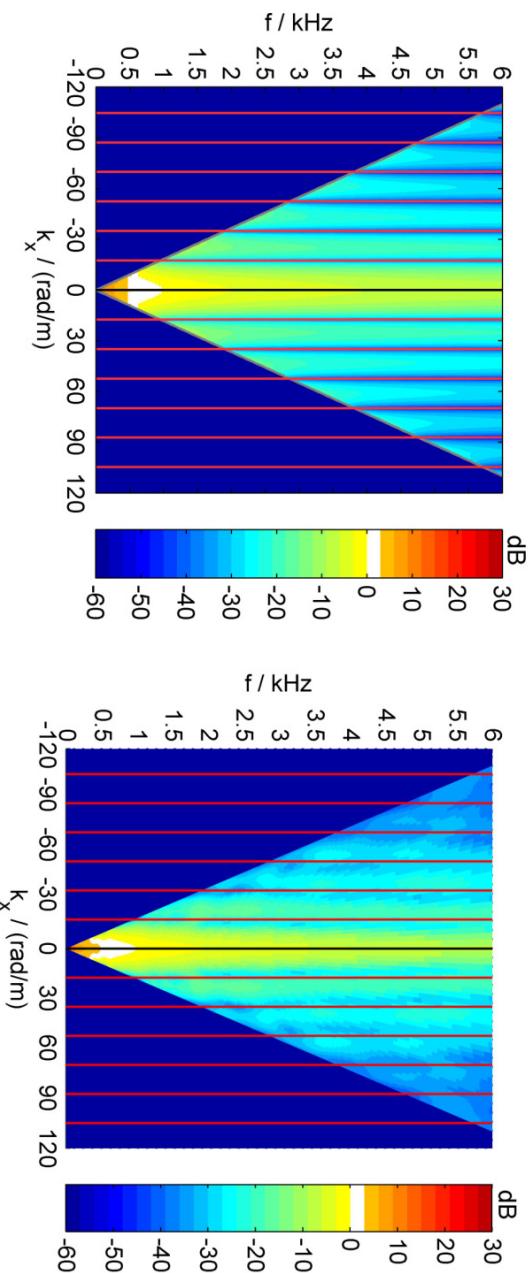
line piston (waveguide)

$$L = \Delta x = 3"$$

$$H_{\text{Circ}}(k_x) = \frac{2 J_1(\frac{\omega}{c} \sin \theta r_0)}{\frac{\omega}{c} \sin \theta r_0}$$

$$H_{\text{Rect}}(k_x) = \frac{\sin\left(\frac{\omega}{c} \sin \theta \frac{L}{2}\right)}{\frac{\omega}{c} \sin \theta \frac{L}{2}}$$

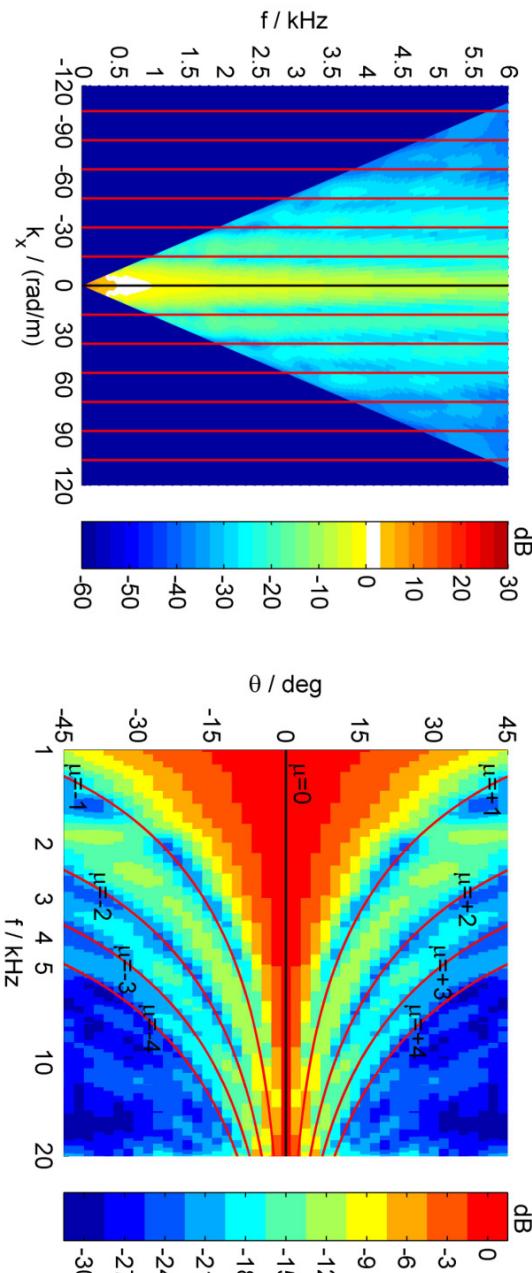
Waveguide Model and Measurement



ideal waveguide model
 $L = \Delta x = 36\text{cm}$

waveguide measurement
 $L = \Delta x = 36\text{cm}$

Waveguide Measurement: Isobars



$$k_x = \frac{2\pi f}{c} \sin \theta$$

Conclusion

WST criteria I & II proved with sound field synthesis and spatial sampling theory

Loudspeakers act as a spatial lowpass filter

Spatial-aliasing-free sound field with a quasi-continuous line source array

- no gaps between waveguides
 - waveguide should match ideal line piston as best as possible
- ⇒ perfect spatial lowpass filter

slides of this talk available @ <http://spatialaudio.net/>

Schultz, F.; Rettberg, T.; Spors, S. (2014): "On Spatial-Aliasing-Free Sound Field Reproduction using Infinite Line Source Arrays". In Proc. of 136th Aud. Eng. Soc. Conv., Berlin. #9078.